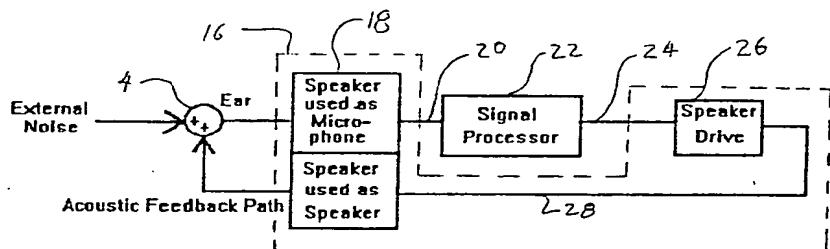




INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 5 : H04B		A2	(11) International Publication Number: WO 94/11953
			(43) International Publication Date: 26 May 1994 (26.05.94)
<p>(21) International Application Number: PCT/US93/10958</p> <p>(22) International Filing Date: 12 November 1993 (12.11.93)</p> <p>(30) Priority data: PL 5792 11 November 1992 (11.11.92) AU</p> <p>(71) Applicant (for all designated States except US): NOISE BUSTER TECHNOLOGY [AU/AU]; 15 Orion Road, Lance Cove, NSW 2066 (AU).</p> <p>(72) Inventors; and</p> <p>(75) Inventors/Applicants (for US only) : TODTER, Chris [US/US]; 4222 Orchard Avenue, San Diego, CA 92106 (US). CLIFTON, Scott [AU/AU]; 53-55 Shepherd Street, Marrickville, NSW 2204 (AU). BREMNER, Paul [AU/AU]; 2 Cray Street, Henley, NSW (AU).</p>		<p>(74) Agent: TIGHE, Thomas, J.; 6265 Greenwich Drive, Suite 250, San Diego, CA 92122 (US).</p> <p>(81) Designated States: AU, CA, DE, GB, JP, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).</p> <p>Published Without international search report and to be republished upon receipt of that report.</p>	
<p>(54) Title: ACTIVE NOISE CANCELLATION SYSTEM</p> <p>(57) Abstract</p> <p>Active noise control systems that heretofore have had at least a microphone which responds to ambient acoustic noise waves and a speaker which transmits an altered version of the ambient noise waves over a frequency range to provide a measure of noise cancellation in the region of the microphone are improved by using a bilateral transducer circuit in place of a separate microphone and speaker. Two embodiments of such ANC systems are disclosed. Three embodiments of a bilateral transducer circuit are disclosed, and in each a bilateral transducer both senses ambient noise and produces acoustic waves to cancel the noise. The electrical interface for each bilateral transducer circuit consists of a speaker input drive signal as an input and a simulated microphone signal as an output. In a first embodiment the drive to the bilateral transducer is periodically turned off at a rate above the hearing frequency limit, and in the "off period" the transducer's drive element is sensed to produce a reverse output signal from which is subtracted a synthesized signal representing the speaker velocity response to the drive signal to produce the simulated microphone signal which is then processed in further active noise circuitry in a known way. In further embodiments the reverse output signal is derived by sensing the energy being sent to the transducer to produce the acoustic waves, or by a separate sensing coil in a coil driven transducer.</p>			



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

ACTIVE NOISE CANCELLATION SYSTEM

BACKGROUND OF THE INVENTION

This invention relates in general to active noise cancellation systems, and in particular to such systems which employ a microphone proximate a listener's ear to receive 5 essentially the same ambient noise received by the ear and a speaker for producing sound in the vicinity of the microphone to cancel the ambient noise.

Prior art as in U.S. Patent 2,972,018 by Hawley et al. (1953) provide for a microphone which responds to ambient noise 10 and a speaker which transmits an altered version of the ambient noise to provide a measure of noise cancellation in the region of the microphone. Virtually all subsequent patents of improvement incorporate some variant of this concept, but they all use microphones.

15 This invention takes advantage of the known fact that certain kinds of speakers (e.g. diaphragm speakers) respond to pressure waves of incoming sound (e.g. ambient noise) and produce an output signal representative of the incoming sound.

20 Other advantages and attributes of this invention will be readily discernable from a reading of the text hereinafter.

SUMMARY OF THE INVENTION

An object of this invention is to provide the means to implement active noise attenuation systems without the need to use a microphone.

25 A further object of this invention is to provide an active noise attenuation system in which a speaker is used as a bilateral transducer, i.e. a transducer that both converts acoustic waves to corresponding electrical energy and converts electrical energy to acoustic waves.

30 These and other objects, which are apparent from this specification, are achieved by an improvement for at least eliminating the microphone from any ANC ("active noise control") device having at least a microphone which responds to

ambient acoustic noise waves and a speaker which transmits an altered version of the ambient noise waves over a frequency range to provide a measure of noise cancellation in the region of the microphone, the improvement comprising: (a) bilateral transducer means, disposed in said region, for converting the acoustic noise waves to a corresponding first signal and for converting a second signal to corresponding acoustic waves; and (b) means for applying a transfer function to the first signal, over said frequency range, resulting in the second signal, the transfer function causing acoustic waves produced by the bilateral transducer to be generally equal in magnitude but opposite in phase to the acoustic noise waves impinging the bilateral transducer. The objects are also achieved by two embodiments of an ANC system. A first embodiment comprises: (a) a bilateral transducer means, disposed proximate a listener so as to be impinged by the same acoustic noise waves to which the listener is subjected, for converting the acoustic noise waves to a corresponding first signal and for converting a second signal to corresponding acoustic waves; and (b) means for applying a transfer function to the first signal, over a frequency range, resulting in the second signal, the transfer function causing acoustic waves produced by the bilateral transducer to be generally equal in magnitude but opposite in phase to the acoustic noise waves impinging the bilateral transducer. A second embodiment comprising: (a) bilateral transducer means, disposed proximate a listener so as to be impinged by the same acoustic noise waves to which the listener is subjected, for converting the acoustic noise waves to a corresponding first signal and for converting a sum signal to corresponding acoustic waves; (b) means for applying a transfer function to the first signal, over a frequency range, resulting in a second signal; (c) a feed forward circuit comprising: (i) acousto-electric transducer means, disposed to be impinged by the same acoustic noise waves to which the listener is subjected for converting the noise waves to a corresponding third signal, and (ii) means for applying a transfer function to the third signal resulting in a fourth signal; and (d) means

for summing the second and the fourth signals to produce the sum signal, the overall transfer function being ideally negative unity over the frequency range.

There are multiple ways of embodying the bilateral transducer
5 means and thus eliminating the need for additional microphones. In a first embodiment the drive to a speaker is periodically turned off at a rate above the hearing frequency limit, and in the "off period" the speaker drive element is sensed by a circuit that produces a signal which is the combination of a
10 signal representing the speaker velocity caused by a speaker drive signal and a signal caused by ambient noise because of the speaker's inherent ability to act as a microphone. The latter signal is separated from the composite to produce a simulated microphone representation of ambient noise which is
15 then processed in further active noise circuitry in a known ways. In further embodiments use is made of a non-zero output impedance of the drive amplifier, across which appears a combination of signals. These signals represent both some measure of the speaker representation of its intended drive
20 signal and the ambient noise impinging the speaker. These signals are separated and the noise component is treated in the normal active noise control manner.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a functional block diagram of a prior art
25 active noise cancellation system.

Figure 2 is a functional block diagram of a first embodiment of an active noise cancellation system according to this invention.

Figure 3 is a functional block diagram of a second embodiment of an active noise cancellation system according to this invention.

Figure 4 is a functional block diagram of a first embodiment of a bilateral transducer circuit according to this invention.

Figure 5 is a functional block diagram of a second embodiment of a bilateral transducer circuit according to this invention.

5 Figure 6 is a functional block diagram of a third embodiment of a bilateral transducer circuit according to this invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring to Figure 1, a basic prior art ANC system is illustrated to have a first transducer 2 in the form of a 10 microphone proximate a listener's ear 4, e.g. inside of an earpiece covering the listener's ear. The microphone is located to receive essentially the same acoustic noise that the ear is receiving and convert this noise into corresponding 15 electrical energy, i.e. electrical signals at the microphone's output 6. These electrical signals are processed by a signal processor 8 to produce speaker drive input signals 10 which are communicated to a speaker driver 12 which in turn sends corresponding electrical drive energy to a second transducer in 20 the form of a speaker 14. The speaker converts the electrical drive energy into corresponding acoustic waves which are directed to impinge the listener's ear. Ideally, the gain in the feedback loop is negative unity such that the acoustic 25 waves impinging the ear from the speaker is at all times equal in magnitude but opposite in phase to that of the ambient noise impinging the ear. The noise and the acoustic waves produced by the speaker are ideally summed to zero at the listener's ear.

Referring to Figure 2, a first embodiment of this invention is illustrated as having the microphone and speaker of Figure 1 replaced by a circuit 16 ("bilateral transducer circuit") having a bilateral transducer. As used herein 30 "bilateral transducer" shall refer to and mean a transducer which produces acoustic waves by means of a vibratory element 35 in response to, and corresponding to, an energization signal applied to the transducer, and which produces a reverse output in response to, and corresponding to, mechanical movement of

the vibratory element not attributable to energization. As illustrated, the bilateral transducer is a speaker 18 disposed in the system to function both as a microphone and a speaker. The bilateral transducer circuit produces a "microphone" output signal 20, a simulated microphone signal, corresponding to ambient noise. The simulated microphone output signal is communicated to a signal processor 22 to produce a corresponding speaker drive input signal 24 which is communicated to a speaker driver 26. The speaker driver produces a corresponding speaker drive signal 28 which causes the bilateral transducer 18 to produce corresponding acoustic waves intended to cancel the ambient noise. As in the conventional ANC of Figure 1, the loop gain is preferably negative unity.

Referring to Figure 3, a second embodiment of this invention is similar to the first embodiment illustrated in Figure 2 in that there exists an acoustic feedback loop utilizing a bilateral transducer circuit 30, but in addition there is a feed forward circuit having a microphone 32 which can be disposed inside or outside of an earpiece (not shown) the output of which is communicated to a first signal processor 34 the output of which is communicated as an input to a signal adder 36. Another input to the adder is the output 38 of a second signal processor 40 which receives as an input a simulated microphone output 42 from the bilateral circuit 30. The sum output of the adder is communicated to the bilateral circuit 30 as a speaker input drive signal 44. Such a feed forward circuit is described in PCT Patent Application No. PCT/US91/06636 by the same inventors as listed herein.

Referring to Figure 4, a first embodiment of a bilateral transducer circuit is illustrated to have a speaker drive input signal 46A from an ANC system (e.g. see 24 and 44 of Figures 2 and 3) communicated to both a speaker drive circuit 48A and a speaker velocity synthesis circuit 50. The speaker drive circuit contains an output stage 52A which produces a speaker drive signal 54A corresponding to the speaker drive input signal. The speaker drive signal is communicated to a speaker

56A in order to cause it to produce acoustic waves intended to cancel ambient noise, but the speaker drive signal is gated "on" and "off" by a "Q" output of an oscillating chopper circuit 58. By "on" it is meant that when Q is logically true,
5 the output of the output stage is enabled so that speaker drive signal is communicated to the input of the speaker; but when Q is logically false, the output of the output stage is disabled and presents only a high impedance to the speaker input. The chopper also provides a sampling clock 60 to a waveform 10 sampling circuit 62 having an input communicating with the input of the speaker. The sampling clock can be, or be derived from, for example the logical compliment of Q. The output 64 of the waveform sampling circuit is communicated to a waveform reconstruction circuit 66, the output of which is communicated 15 to a signal subtractor 68 which subtracts therefrom the output 70 of the speaker velocity synthesis circuit 50 to produce a simulated microphone output 72A for use in an ANC system (e.g. see 20 and 42 of Figures 2 and 3).

20 The bilateral transducers can be diaphragm speakers with coil drives of conventional design because it is well known that they generate electrical energy corresponding and in response to mechanical movement of the diaphragms by external forces, such as ambient acoustic waves. Alternately, the bilateral transducers can be piezofilm transducers which 25 basically are each a diaphragm coated with capacitive electrodes that can be made to bend or vibrate by input of electrical signals. A piezofilm transducer is inherently bilateral in that if the diaphragm is bent or stretched as in vibration, it generates an output voltage. The latter has 30 significant advantage because by applying the electrodes strategically to benefit on the surface of the diaphragm, it is possible to alter or affect or correct some of the undesirable resonance modes of a standard diaphragm, thus improving the performance of the system of this invention. The generated 35 electrical energy is felt across the input terminals of the speakers' drive elements, e.g. the terminals of drive coils and piezofilm coatings.

Referring again to Figure 4, the chopper circuit 58 preferably oscillates at a high frequency relative to audible sound, for example 100 kilohertz, which is sufficiently above the audible sound range to negligibly effect the noise cancellation. During the times that the speaker drive signal is gated off, the electrical energy generated by the speaker (which can be called the speaker's "reverse output") corresponds to the speaker's diaphragm velocity which is the algebraic sum of a velocity component caused by the speaker drive signal just gated off plus any velocity component due to impinging acoustic noise waves. The waveform sampling circuit 62 samples the speaker's reverse output in response to each sampling clock and communicates the samples in real time to the waveform reconstruction circuit 66 which can be a low pass filter. By this technique, the output of the reconstruction circuit is a signal which corresponds in real time to the algebraic sum of the two diaphragm velocity components. The reverse output signal also corresponds to the algebraic sum of the acoustic waves being created by the diaphragm due to the drive signal 54A and the acoustic noise waves impinging the diaphragm. The speaker velocity synthesis circuit 50 produces a frequency dependent signal 70 corresponding to what the speaker's velocity response would be to the speaker drive input signal 46A without any external noise components, and therefore also corresponding to the acoustic waves being created by the diaphragm. By subtracting the synthesized signal from the reverse output signal, the simulated microphone output 72A is ideally a signal which corresponds only to the acoustic noise impinging the speaker's diaphragm.

Referring to Figure 5, a second embodiment of a bilateral transducer circuit is illustrated to have a speaker output stage 52B which receives as an input a speaker drive input signal 46B from an ANC system (e.g. see 24 and 44 of Figures 2 and 3). The output stage produces a speaker drive signal 54B corresponding to the speaker drive input signal. The speaker drive signal is communicated to a speaker 56B in order to cause it to produce acoustic waves intended to cancel ambient noise.

A sensing circuit 74 continuously senses the level of current in the signal path between the output stage and the speaker and produces a signal 76 ("current level signal") corresponding thereto. The sensing circuit can, for example, be a linear 5 circuit having a differential input of relatively high impedance (so as not to unduly load the signal path) connected across the output impedance of the output stage. The current in the signal path at any given time is the algebraic sum of the current of the speaker drive signal 54B and the speaker's 10 reverse output current, and therefore the current level signal corresponds in real time to the algebraic sum of the diaphragm velocity component caused by the speaker drive signal 54B and the velocity component due to impinging acoustic noise waves. As in Figure 4, the speaker's velocity response to the speaker 15 drive input signal 46B is synthesized in real time by a circuit 78 which produces a synthesized velocity signal 80 which is subtracted from the current level signal by a subtractor 82 to produce the simulated microphone output 72B for use in an ANC system (e.g. see 20 and 42 of Figures 2 and 3). By subtracting 20 the synthesized signal from the current level signal, the simulated microphone output 72A is ideally a signal which corresponds only to the acoustic noise impinging the speaker's diaphragm.

Referring to Figure 6, a third embodiment of a bilateral 25 transducer circuit is illustrated to have a speaker output stage 52C which receives as an input a speaker drive input signal 46C from an ANC system (e.g. see 24 and 44 of Figures 2 and 3). The output stage produces a speaker drive signal 54C corresponding to the speaker drive input signal. The speaker 30 drive signal is communicated to a speaker 56C in order to cause it to produce acoustic waves intended to cancel ambient noise. The speaker has a drive coil of conventional design but also has a sensing coil wound along therewith (not shown) for providing a speaker reverse output signal 84 ("sensing coil 35 signal") that is dependent on the speaker diaphragm velocity and inductive coupling between the speaker drive coil (not shown) and the sensing coil. To remove the effects of the

inductive coupling from the sensing coil signal, a signal 86 produced by a speaker inductance synthesizing circuit 88 is subtracted from the sensing coil signal by means of subtractor 90. The speaker inductance synthesizer is responsive to the 5 speaker drive input signal 46C and the signal produced thereby simulates the signal induced in the sensing coil by the speaker drive coil. As in Figures 4 and 5, the speaker's velocity response is synthesized by a circuit 92 that produces a synthesized signal 94 that is also subtracted from the sensing 10 coil signal by subtractor 90 to finally arrive at a simulated microphone signal 72C which ideally corresponds only to the acoustic noise impinging the speaker's diaphragm.

Each of the speaker velocity synthesizers described above can be an implementation of a transfer function based on a 15 known model of the speaker. The speakers of this invention can be modeled by known techniques. For example, a speaker can be characterized by applying known drive signals, within a selected frequency band, to the speaker's drive element while measuring the diaphragm's velocity. Preferably the known drive 20 signals are random signals simulating noise over the frequency band in order to more accurately model the speaker for noise cancellation. From this the transfer function of the speaker can be determined and a synthesizer (e.g. a network of gain and phase shifting elements) can be designed therefrom using 25 conventional design techniques. Likewise the speaker inductance synthesizer 88 of Figure 6 can be designed and implemented in similar fashion. For example, the inductive coupling can be characterized by applying known drive signals, e.g. simulated random signals, within a selected frequency 30 band, to the speaker's drive element while measuring the sensing coil signals. Alternatively, the synthesizers can each be implemented in a long term adaptive circuit varied in near real time.

While two embodiments of ANC systems having bilateral 35 transducer circuits were described, the use of the bilateral transducer circuits is not limited to these ANC embodiments, but rather a bilateral transducer circuit according to this

-10-

invention can be used to improve any device having at least a microphone which responds to ambient acoustic noise waves and a speaker which transmits an altered version of the noise waves over a frequency range to provide a measure of noise cancellation in the region of the microphone. One improvement is the elimination of the microphone. Other improvements and advantages are that the use of a speaker in a bilateral sense, that is as both a speaker and a microphone, first of all puts the sensing surface co-planar with the speaker, and secondly tends to inverse frequency characteristics of the speaker which helps to compensate for speaker resonances and other undesirable characteristics.

The foregoing description and drawings were given for illustrative purposes only, it being understood that the invention is not limited to the embodiments disclosed, but is intended to embrace any and all alternatives, equivalents, modifications and rearrangements of elements falling within the scope of the invention as defined by the following claims.

WE CLAIM:

CLAIMS

1. For a device having at least a microphone which responds to
2 ambient acoustic noise waves and a speaker which transmits an
4 altered version of the ambient noise waves over a frequency
6 range to provide a measure of noise cancellation in the region
of the microphone, an improvement for at least eliminating the
microphone comprising:

8 (a) bilateral transducer means, disposed in said
region, for converting the acoustic noise waves to a
10 corresponding first signal and for converting a second
signal to corresponding acoustic waves, and

12 (b) means for applying a transfer function to the
first signal, over said frequency range, resulting in the
14 second signal, the transfer function causing acoustic
waves produced by the bilateral transducer to be generally
16 equal in magnitude but opposite in phase to the acoustic
noise waves impinging the bilateral transducer.

2. The improvement according to claim 1 wherein the bilateral
2 transducer means comprises:

4 (a) bilateral transducer having a common port for
energization and reverse output,

6 (b) means for energizing the bilateral transducer in
response to and corresponding to said second signal,

8 (c) means for periodically de-energizing the
bilateral transducer at a rate high above a normal audible
frequency limit,

10 (d) means for sampling the common port during times
when the bilateral transducer is de-energized,

12 (e) means for receiving the samples and constructing
therefrom a reverse output signal,

14 (f) means for receiving said second signal and
16 synthesizing therefrom a signal representative of what the
bilateral transducer's velocity response would be to said
18 second signal in the absence of said ambient acoustic
noise waves, and

20 (g) means for subtracting the synthesized signal from the reverse output signal, the difference being said first signal.

3. The improvement according to claim 1 wherein the bilateral
2 transducer means comprises:

4 (a) a bilateral transducer having a common port for
energization and reverse output,

6 (b) drive means for providing energy to said port via
a signal path in response to and corresponding to said
second signal,

8 (c) sensing means for continuously measuring the
energy level in said signal path and producing a signal
10 corresponding thereto,

12 (d) means for receiving said second signal and
synthesizing therefrom a signal representative of what the
bilateral transducer's velocity response would be to said
14 second signal in the absence of said ambient acoustic
noise waves, and

16 (e) means for subtracting the synthesized signal from
the signal produced by the sensing means, the difference
18 being said first signal.

4. The improvement according to claim 1 wherein the bilateral
2 transducer means comprises:

4 (a) a bilateral transducer having a drive coil and a
sensing coil for producing a reverse output signal,

6 (b) means for energizing the drive coil in response to and corresponding to said second signal,

8 (c) means for receiving said second signal and
synthesizing therefrom a signal representative of a signal
induced in the sensing coil by the drive coil,

10 (d) means for receiving said second signal and
11 synthesizing therefrom a signal representative of what the
12 bilateral transducer's velocity response would be to said
13 second signal in the absence of said ambient acoustic
14 noise waves, and

16 (e) means for subtracting both synthesized signals
from the reverse output signal, the difference being said
first signal.

5. A device for canceling acoustic noise in the vicinity of a
2 listener comprising:

4 (a) a bilateral transducer means, disposed proximate
the listener so as to be impinged by the same acoustic
6 noise waves to which the listener is subjected, for
converting the acoustic noise waves to a corresponding
8 first signal and for converting a second signal to
corresponding acoustic waves, and

10 (b) means for applying a transfer function to the
first signal, over a frequency range, resulting in the
12 second signal, the transfer function causing acoustic
waves produced by the bilateral transducer to be generally
14 equal in magnitude but opposite in phase to the acoustic
noise waves impinging the bilateral transducer.

6. The device according to claim 5 wherein the bilateral
2 transducer means comprises:

4 (a) a bilateral transducer having a common port for
energization and reverse output,

6 (b) means for energizing the bilateral transducer in
response to and corresponding to said second signal,

8 (c) means for periodically de-energizing the
bilateral transducer at a rate high above a normal audible
frequency limit,

10 (d) means for sampling the common port during times
when the bilateral transducer is de-energized,

12 (e) means for receiving the samples and constructing
therefrom a reverse output signal,

14 (f) means for receiving said second signal and
16 synthesizing therefrom a signal representative of what the
bilateral transducer's velocity response would be to said
18 second signal in the absence of said ambient acoustic
noise waves, and

20 (g) means for subtracting the synthesized signal from
the reverse output signal, the difference being said first
signal.

2 7. The device according to claim 5 wherein the bilateral
transducer means comprises:

4 (a) a bilateral transducer having a common port for
energization and reverse output,

6 (b) drive means for providing energy to said port via
a signal path in response to and corresponding to said
second signal,

8 (c) sensing means for continuously measuring the
energy level in said signal path and producing a signal
corresponding thereto,

10 (d) means for receiving said second signal and
12 synthesizing therefrom a signal representative of what the
14 bilateral transducer's velocity response would be to said
second signal in the absence of said ambient acoustic
noise waves, and

16 (e) means for subtracting the synthesized signal from
the signal produced by the sensing means, the difference
18 being said first signal.

8. The device according to claim 5 wherein the bilateral
2 transducer means comprises:

2 (a) a bilateral transducer having a drive coil and a
4 sensing coil for producing a reverse output signal,

6 (b) means for energizing the drive coil in response
to and corresponding to said second signal,

8 (c) means for receiving said second signal and
8 synthesizing therefrom a signal representative of a signal
induced in the sensing coil by the drive coil,

10 (d) means for receiving said second signal and
12 synthesizing therefrom a signal representative of what the
14 bilateral transducer's velocity response would be to said
second signal in the absence of said ambient acoustic
noise waves, and

16 (e) means for subtracting both synthesized signals
from the reverse output signal, the difference being said
first signal.

2 9. A device for canceling acoustic noise in the vicinity of a
listener comprising:

4 (a) bilateral transducer means, disposed proximate
the listener so as to be impinged by the same acoustic
6 noise waves to which the listener is subjected, for
converting the acoustic noise waves to a corresponding
8 first signal and for converting a sum signal to
corresponding acoustic waves,

10 (b) means for applying a transfer function to the
first signal, over a frequency range, resulting in a
second signal,

12 (c) a feed forward circuit comprising:

14 (i) acousto-electric transducer means, disposed
to be impinged by the same acoustic noise waves to
which the listener is subjected for converting the
16 noise waves to a corresponding third signal,

18 (ii) means for applying a transfer function to
the third signal resulting in a fourth signal,

20 and (d) means for summing the second and the fourth
signals to produce the sum signal, the overall transfer
22 function being ideally negative unity over the frequency
range.

10. The device according to claim 9 wherein the bilateral
2 transducer means comprises:

4 (a) a bilateral transducer having a common port for
energization and reverse output,

6 (b) means for energizing the bilateral transducer in
response to and corresponding to said second signal,

8 (c) means for periodically de-energizing the
bilateral transducer at a rate high above a normal audible
frequency limit,

-16-

10 (d) means for sampling the common port during times
when the bilateral transducer is de-energized,
12 (e) means for receiving the samples and constructing
therefrom a reverse output signal,
14 (f) means for receiving said second signal and
synthesizing therefrom a signal representative of what the
16 bilateral transducer's velocity response would be to said
second signal in the absence of said ambient acoustic
18 noise waves, and
20 (g) means for subtracting the synthesized signal from
the reverse output signal, the difference being said first
signal.

11. The device according to claim 9 wherein the bilateral
2 transducer means comprises:

4 (a) a bilateral transducer having a common port for
energization and reverse output,
6 (b) drive means for providing energy to said port via
a signal path in response to and corresponding to said
second signal,
8 (c) sensing means for continuously measuring the
energy level in said signal path and producing a signal
10 corresponding thereto,
12 (d) means for receiving said second signal and
synthesizing therefrom a signal representative of what the
14 bilateral transducer's velocity response would be to said
second signal in the absence of said ambient acoustic
noise waves, and
16 (e) means for subtracting the synthesized signal from
the signal produced by the sensing means, the difference
18 being said first signal.

12. The device according to claim 9 wherein the bilateral
2 transducer means comprises:

4 (a) a bilateral transducer having a drive coil and a
sensing coil for producing a reverse output signal,

6 (b) means for energizing the drive coil in response
to and corresponding to said second signal,

8 (c) means for receiving said second signal and
synthesizing therefrom a signal representative of a signal
induced in the sensing coil by the drive coil,

10 (d) means for receiving said second signal and
synthesizing therefrom a signal representative of what the
12 bilateral transducer's velocity response would be to said
second signal in the absence of said ambient acoustic
14 noise waves, and

16 (e) means for subtracting both synthesized signals
from the reverse output signal, the difference being said
first signal.

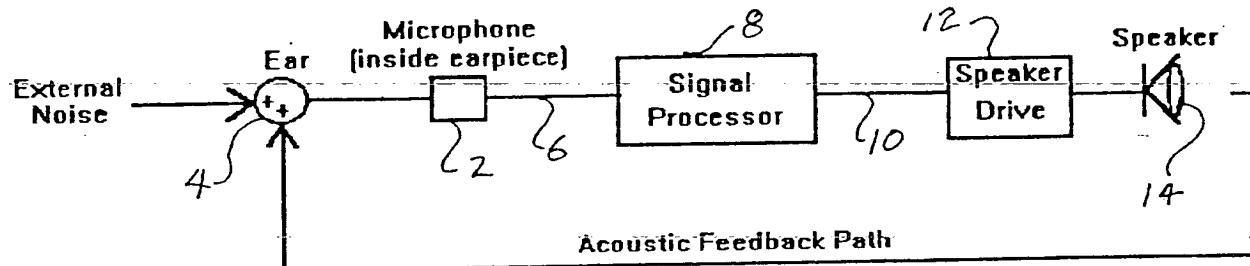


FIG. 1 PRIOR ART

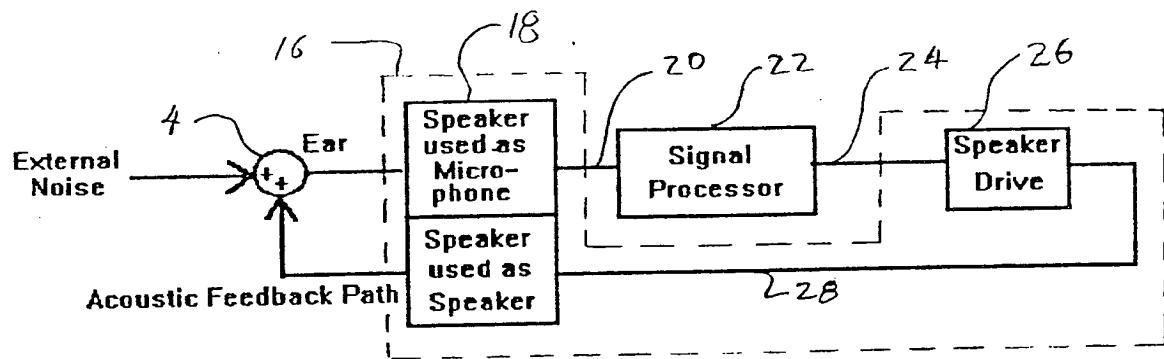


FIG. 2

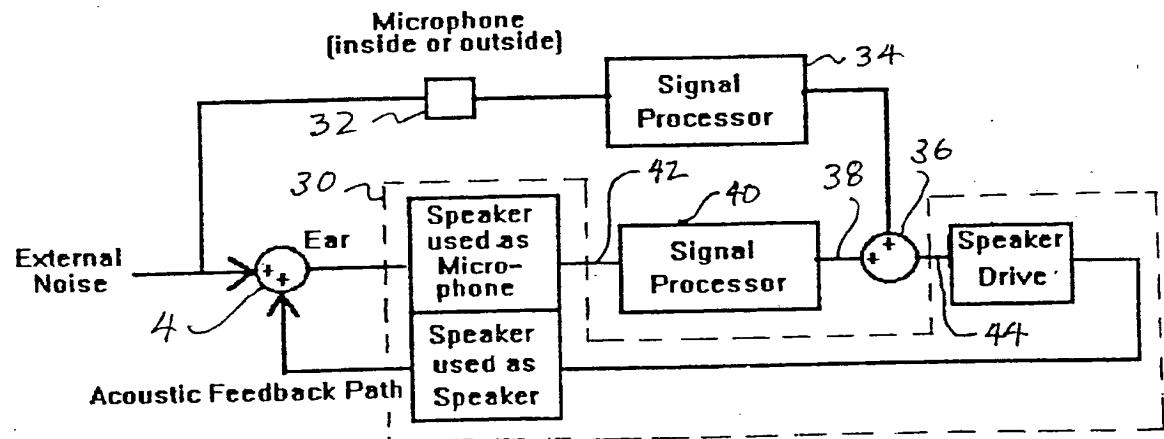


FIG. 3

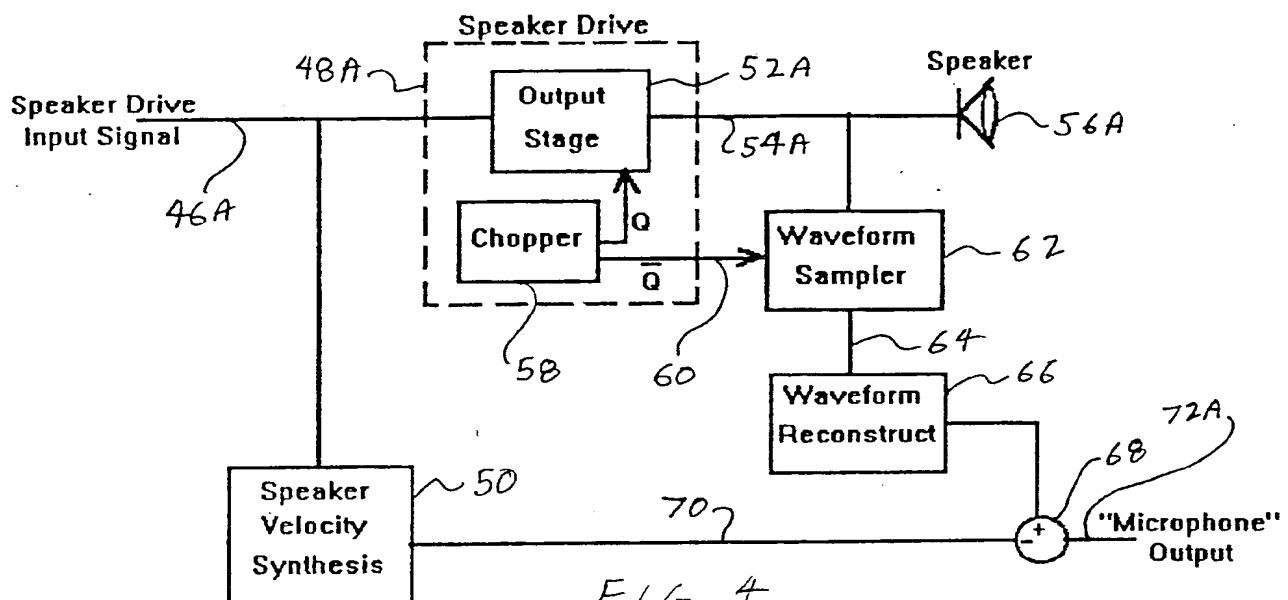


FIG. 4

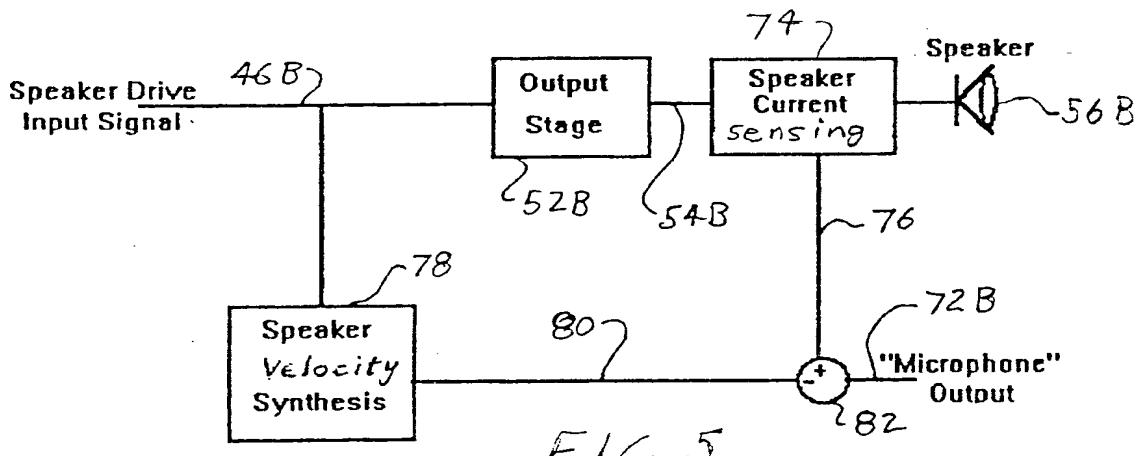


FIG. 5

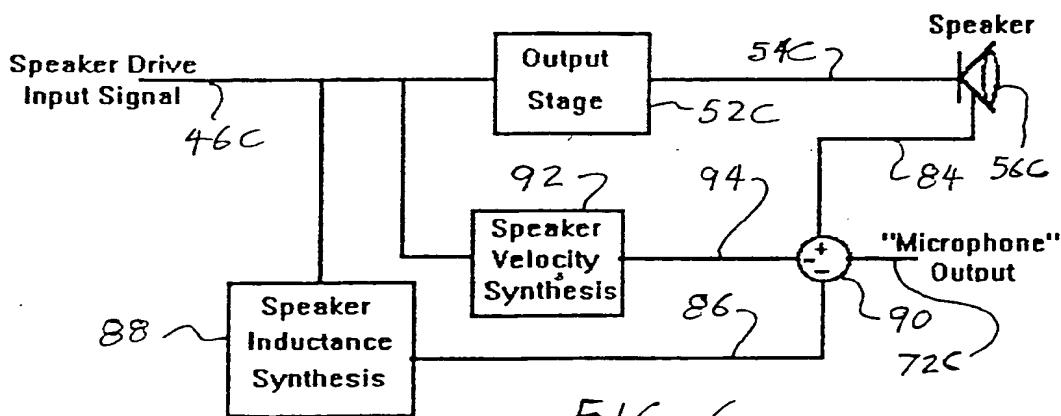


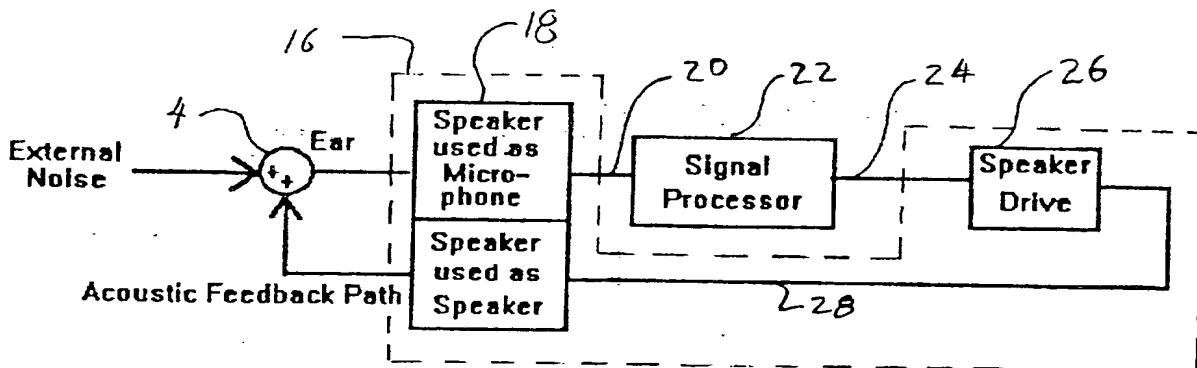
FIG. 6

THIS PAGE BLANK (USPTO)

INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 5 : A61F 11/06		A3	(11) International Publication Number: WO 94/11953 (43) International Publication Date: 26 May 1994 (26.05.94)
(21) International Application Number: PCT/US93/10958 (22) International Filing Date: 12 November 1993 (12.11.93)		(74) Agent: TIGHE, Thomas, J.; 6265 Greenwich Drive, Suite 250, San Diego, CA 92122 (US).	
(30) Priority data: PL 5792 11 November 1992 (11.11.92) AU		(81) Designated States: AU, CA, DE, GB, JP, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).	
(71) Applicant (for all designated States except US): NOISE BUSTER TECHNOLOGY [AU/AU]; 15 Orion Road, Lance Cove, NSW 2066 (AU).		Published <i>With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>	
(72) Inventors; and (75) Inventors/Applicants (for US only) : TODTER, Chris [US/US]; 4222 Orchard Avenue, San Diego, CA 92106 (US). CLIFTON, Scott [AU/AU]; 53-55 Shepherd Street, Marickville, NSW 2204 (AU). BREMNER, Paul [AU/AU]; 2 Cray Street, Henley, NSW (AU).		(88) Date of publication of the international search report: 7 July 1994 (07.07.94)	

(54) Title: ACTIVE NOISE CANCELLATION SYSTEM



(57) Abstract

A bilateral transducer (18) for use in an active noise cancellation system both senses ambient noise and produces signal as an input and a simulated microphone signal as an output. In a first embodiment, the drive signal to the bilateral transducer is periodically turned off at a rate above audibility, and in the "off period" the transducer's drive element is sensed to produce a reverse output signal from which is subtracted a synthesized signal representing the speaker velocity. The response to the drive signal is produced by the transducer to produce the acoustic waves, or by a separate sensing signal is derived by sensing the energy being sent to the transducer to produce the acoustic waves, or by a separate sensing

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BC	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TC	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

A. CLASSIFICATION OF SUBJECT MATTER

IPC(5) :A61F 11/06

US CL :381/71

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 381/71, 96

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

APS

search terms bilateral transducer#

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US, A, 4,985,925 (LANGBERG et al.) 15 January 1991, Figures 2, 4 and 6 and accompanying text.	1,3,5,7
Y	US, A, 4,243,839 (TAKAHASHI et al.) 06 January 1981, Figure 1.	8
X,E	US,A, 5,267,321 (LANGBERG) 30 November 1993, Figure 2.	1,3,5,7

Further documents are listed in the continuation of Box C.

See patent family annex.

Special categories of cited documents:	
"A"	document defining the general state of the art which is not considered to be part of particular relevance
"E"	earlier document published on or after the international filing date
"L"	document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
"O"	document referring to an oral disclosure, use, exhibition or other means
"P"	document published prior to the international filing date but later than the priority date claimed
"T"	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"X"	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"Y"	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"&"	document member of the same patent family

Date of the actual completion of the international search

05 MAY 1994

Date of mailing of the international search report

10 MAY 1994

Name and mailing address of the ISA/US
Commissioner of Patents and Trademarks
Box PCT
Washington, D.C. 20231

Facsimile No. (703) 305-3230

Authorized officer

MARK KELLY

Telephone No. (703) 305-4700

Form PCT/ISA/210 (second sheet)(July 1992)*

THIS PAGE BLANK (USPTO)

**This Page is Inserted by IFW Indexing and Scanning
Operations and is not part of the Official Record**

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- BLACK BORDERS**
- IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- FADED TEXT OR DRAWING**
- BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- SKEWED/SLANTED IMAGES**
- COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- GRAY SCALE DOCUMENTS**
- LINES OR MARKS ON ORIGINAL DOCUMENT**
- REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- OTHER:** _____

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.

THIS PAGE BLANK (USPTO)